

PHASOR STATE ESTIMATION

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Outline

- Phasor State Estimation (PSE)
 - PSE Concept
 - PSE with and without Redundancy
- PSE Model and Implementation
 - Problem Formulation
 - Weighted Nonlinear Least Squares
 - Application to the Marcy-Massena Transfer Path
- Angle-Bias Correction with PSE
 - Angle-Bias Errors on PDC PMU Data
 - Angle-Bias Detection Extension of the PSE Model
- Further Work
- References

Phasor State Estimation (i)

- Concept and Applications
 - Hybrid State Estimation



- Phasor State Estimator is independent of the SE, and supported only by a limited number of PMUs
 - Added reliability when the SE is functional
 - Provide observability of the HV network when the SE is not available.
 - Functions:
 - Provide estimates for unmonitored buses
 - Detect bad PMU data (Angle-biases)
 - Provide a platform to develop monitoring and control applications

Phasor State Estimation (ii)



PSE without Redundancy



Problem Formulation (i)

- We formulate the problem as a Weighted Least Squares problem.
- This requires to construct a model containing:

The Synchrophasor Measurements, and

- The network model (transmission lines, transformers, etc.)
- The state-variables of the model and the measurements should be explicit in the formulation.
- Sum of squares solution should be reliable and fast.
- Inherent data errors should be be detected and corrected.

Problem Formulation (ii)

Measurement Model:

We construct the voltage and current magnitude, and angle equations at each PMU-measured Bus (i) as follows:



Problem Formulation (iii)

Network Model:

Complex KVL Network Equations for each PMU-Bus:

For
$$k = 1$$
 to N
 $\tilde{V}_{i_k} = \tilde{V}_{j_k} + \tilde{Z}_{ij_k}\tilde{I}_{i_k}$

- Separate the equation in real and imaginary parts.
- This generates two network equations per PMU-Bus.
- Use Least Squares to estimate X from the network and measurement equations.

$$\mathbf{x} = \begin{bmatrix} V_i & I_i & | V_{j_k} & I_{j_k} & | \theta_i & \delta_{i_k} & | \theta_{j_k} & \delta_{j_k} \end{bmatrix}^T$$

- □ A linear weighted LS can be designed, but it will not solve directly for the states above → does not relate directly to the measurements.
- □ A weighted nonlinear least squares is formulated.

Weighted Nonlinear Least Squares (i)

Nonlinear Least Squares:

Sum of squares measure for data fitting

$$\min_{\mathbf{x}(t)} q(\mathbf{x}(t)) = \frac{1}{2} \sum_{i=1}^{m} \left[w_i f_i(\mathbf{x}(t)) \right]^2, \quad \mathbf{x} \in \mathbb{R}^n$$

• Where $f_i(\mathbf{x}(t))$ are the network and measurement equations

Iterative Gauss-Newton Solution:

Descent Direction:
$$\mathbf{H} = \left[\left\{ \mathbf{W} \mathbf{J} \left(\mathbf{x}^{(k)} \right) \right\}^T \mathbf{W} \mathbf{J} \left(\mathbf{x}^{(k)} \right) \right]^{-1}$$

$$\mathbf{s}^{(k)} = -\mathbf{H} \left(\mathbf{W} \mathbf{J} \left(\mathbf{x}^{(k)} \right) \right)^T \mathbf{W} \mathbf{f} \left(\mathbf{x}^{(k)} \right)$$
Solution Update:
$$\mathbf{x}^{(k+1)} = \mathbf{x}^{(k)} + \mathbf{s}^{(k)}$$

k denotes the number of iteration.

Weighted Nonlinear Least Squares (ii)

 \square WLS Solution includes W:

State vector update:

$$\mathbf{s}^{(k)} = -\mathbf{H}\left(\mathbf{W} \mathbf{J}\left(\mathbf{x}^{(k)}
ight)
ight)^T \mathbf{W} \mathbf{f}\left(\mathbf{x}^{(k)}
ight)$$

W does not change at each iteration.

It is updated for each set of measurements, and is computed from PMU Data for each set n of synchrophasors (a "snapshot").

NY Marcy-Massena Transfer Path (i)



NY Marcy-Massena Transfer Path (ii)



Application to the ML-MA Transfer Path

Marcy-Massena Transfer Path Equivalent Circuit



- Build a model containing the network and the measurement data.
- Network Model:

Calculate $\hat{\tilde{V}}_3$ from \tilde{V}_1 and \tilde{V}_2 :

$$\mathsf{LHS:} \ \hat{\tilde{V}}_{\mathbf{3}} = \underbrace{\left(1 + \tilde{Z}_1 \frac{\tilde{Y}}{2}\right)}_{\tilde{Z}_{\gamma}} \tilde{V}_1 - \tilde{Z}_1 \tilde{I}_1 \qquad \mathsf{RHS:} \ \hat{\tilde{V}}_{\mathbf{3}} = \tilde{V}_2 + \tilde{Z}_{T1} \tilde{I}_{T1} \\ \hat{\tilde{V}}_{\mathbf{3}} = \tilde{V}_2 + \tilde{Z}_{T2} \tilde{I}_{T2}$$

Performance of the WLS for a Single Measurement

Voltage Magnitude Convergence

Voltage Angle Convergence





Performance of the WLS for a Single Measurement

Current Magnitude Convergence $I_1(Est.)$ Current Magnitude (pu) 10.3625 10.362 10.3615 10.361 3 2 1 4 5 Iteration No. $I_{T1}(Est.)$ Current Magnitude (pu) 5.2349 5.2349 5.2349 5.2349 5.2349 5.2349 2 3 4 5 1 Ô Iteration No. $I_{T2}(Est.)$ Current Magnitude (pu)

2

Iteration No.

3

4

5

1

4.8564

4.8562

4.856

4.8558 0



Iteration No.

Current Angle Convergence





Estimated and Measured Current Angles



Difference Between the WLS Estimate and Measurement of the System States: $\Delta x_i = \hat{x}_i - x_{im}$



Angle-Bias Errors on PDC PMU Data

What kind of angle-bias can the PSE correct?

- Angle-biases due to communication delays
- And the implementation of the Bus angle calculation of each manufacturer.
- Observed Angle-Bias in AEP



Angle-Bias Detection and Correction

Extension to the PSE Model

Modify the angle measurement equations as follows:

For each PMU-Bus $i \neq 1$

$$f_{i_{\theta}}^{*}:\theta_{i}-\theta_{im}+\Omega_{si}=0$$

Modified Voltage Angle Measurement Equations

 $f^*_{i_k\delta}:\delta_{i_k}-\delta_{i_km}+\Omega_{si}=0$ Modified Current Angle Measurement Equations

- The new Jacobian elements have to be accounted for.
- Achievable if the Angle-Bias Condition is satisfied.
 - Total number of equations is greater or equal to the total number of unknowns including angle-bias variables:

$$N_T \ge U_T$$

Performance of the WLS for a Single Measurement – Case for an Angle Shift of 15° on Bus 2











Difference Between the WLS Estimate and Measurement of the System States: $\Delta x_i = \hat{x}_i - x_{im}$



On-going and Further Work

Observability Analysis

- H Matrix Conditions
 - PMUs needed for full observability
 - PMUs needed for full angle-bias observability
 - PMUs needed for PSE with Calibration
- Observability of Islanded Sections of the HV Network
- Phasor State Estimation with Calibration
 - Taking windows of data to calibrate scaling factors of PTs and CTs

References

- F. C. Schweppe and J. Wildes, "Power System Static-State Estimation, Part I, II and III", IEEE Transacitons on Power Apparatus and Systems, Vol. PAS-89, Jan. 1970, pp. 120-125.
- A. G. Phadke, J. S. Thorp, and K. J. Karimi, "State Estimlation with Phasor Measurements," *Power Systems, IEEE Transactions on*, vol.1, no.1, pp.233-238, Feb. 1986.
- R. D. Masiello and F. C. Schweppe, "A Tracking Static State Estimator," *IEEE Transactions on Power Apparatus and Systems*, vol.PAS-90, no.3, pp.1025-1033, May 1971.
- H. Modir and R. A Schlueter, "A Dynamic State Estimator for Power System Dynamic Security Assessment", Automatica, Vol. 20, No. 2, pp. 189-199, 1984
- S. Zhong and Ali Abur, "Combined State Estimation and Measurement Calibration", IEEE Transactions on Power Systems, Vol. 20, No. 1, February 2005.
 A. Monticelli, State Estimation in Electric Power Systems. Norwell, MA: Kuwer, 1999.
- A. Abur and A. Gomez-Exposito, Power System State Estimation. New York, NY: Marcel-Dekker, 2004.
- S. G. Nash and A. Sofer, *Linear and Nonlinear Programming*. New York, NY: McGraw-Hill, 1996.
- R. W. Farebrother, *Linear Least Squares Computations*. New York, NY: Marcel-Dekker, 1988.
- A. Bjorck, Numerical Methods for Least Squares Problems. Philadelphia, PA: SIAM, 1996.