

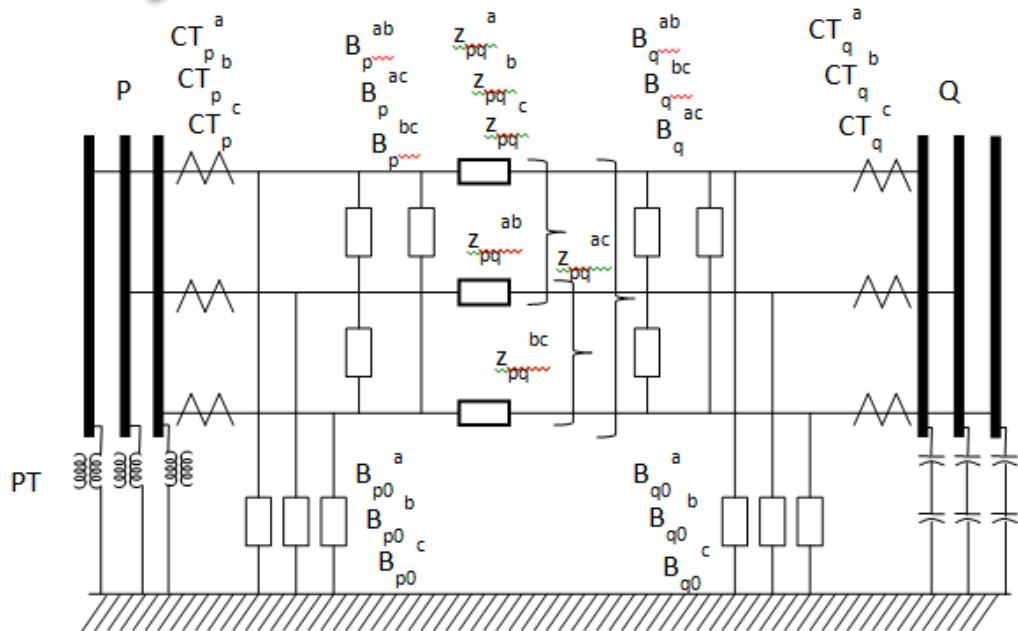


Three-phase Instrument Transformer Calibration with Synchronized Phasor Measurements

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Two-bus system

- Voltages: PT CVT
- Currents: CT
- PMUs are installed at two substations



$$\begin{bmatrix} E_{q0}^a \\ E_{q0}^b \\ E_{q0}^c \end{bmatrix} = \begin{bmatrix} E_{p0}^a \\ E_{p0}^b \\ E_{p0}^c \end{bmatrix} - \begin{bmatrix} Z_{pq}^a & Z_{pq}^{ab} & Z_{pq}^{ac} \\ Z_{pq}^{ab} & Z_{pq}^b & Z_{pq}^{bc} \\ Z_{pq}^{ac} & Z_{pq}^{bc} & Z_{pq}^c \end{bmatrix} \left(\begin{bmatrix} I_{pq0}^a \\ I_{pq0}^b \\ I_{pq0}^c \end{bmatrix} - \begin{bmatrix} B_p^a & B_p^{ab} & B_p^{ac} \\ B_p^{ab} & B_p^b & B_p^{bc} \\ B_p^{ac} & B_p^{bc} & B_p^c \end{bmatrix} \begin{bmatrix} E_{p0}^a \\ E_{p0}^b \\ E_{p0}^c \end{bmatrix} \right)$$

Measurement Errors

- Relaying instrument transformers have 3% to 10% Ratio Magnitude Error and 0.5 to 3 degrees Phase angle Error.

Limits of ratio error relay class	@ rated current	@ 20 times
C and T classification	3%	10%
X classification	1%	user defined

- High accuracy voltage transformers for extra-high voltage (500KV in Dominion Power System) have $\leq 0.15\%$ Ratio Magnitude Error and ≤ 0.1 degrees Phase angle Error.
- Synchronous Phasor Measurements have two parts of error:
 - quantization of the A/D converter (12 bits $\rightarrow 10^{-5}$)
 - GPS synchronization uncertainties ($1\mu\text{s} \rightarrow 0.021$ degress)

Error Models

- Error model of CVTs and CTs:

$$\begin{bmatrix} E^a \\ E^b \\ E^c \end{bmatrix} = \begin{bmatrix} e^a & 0 & 0 \\ 0 & e^b & 0 \\ 0 & 0 & e^c \end{bmatrix} \begin{bmatrix} E_m^a \\ E_m^b \\ E_m^c \end{bmatrix} \quad \begin{bmatrix} I^a \\ I^b \\ I^c \end{bmatrix} = \begin{bmatrix} i^a & 0 & 0 \\ 0 & i^b & 0 \\ 0 & 0 & i^c \end{bmatrix} \begin{bmatrix} I_m^a \\ I_m^b \\ I_m^c \end{bmatrix}$$

Here, **e** and **i** are the ratio correction factor (RCF),

$|e|, |i| \sim \text{Uniform}(0.96, 1.04)$,

$\text{angle}(e), \text{angle}(i) \sim \text{Uniform}(-3, 3)$ degree

Assumption:

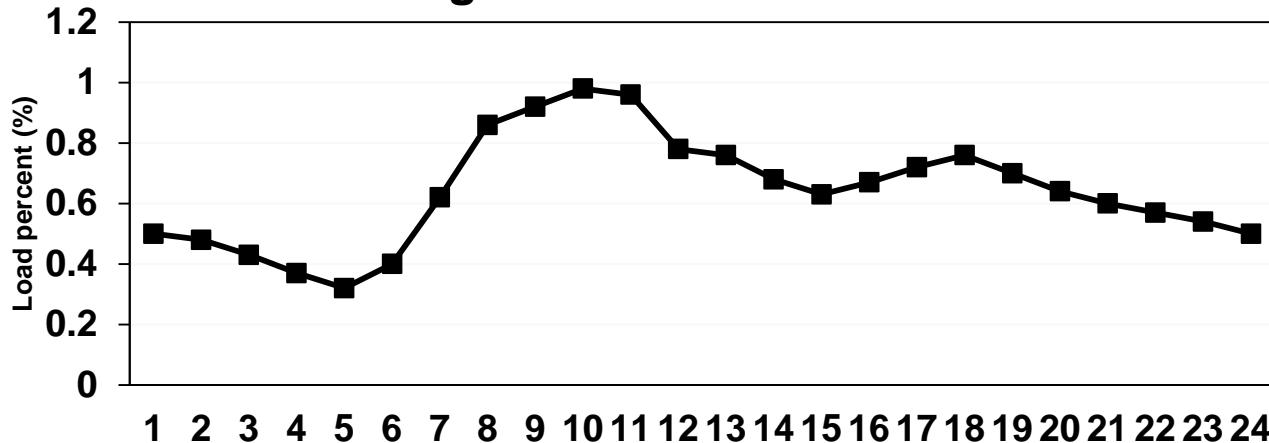
1. The transformer ratio correction factors are assumed to be constant over the simulation period
2. The system model (network impedance matrix) is accurate.

24-hour load cases

- At each point, the load condition changes. PMUs can measure three-phase voltages and currents under each condition. And all of these set satisfy OHM law.

$$\begin{bmatrix} e^a & 0 & 0 \\ 0 & e^b & 0 \\ 0 & 0 & e^c \end{bmatrix} \begin{bmatrix} E_{qm}^a \\ E_{qm}^b \\ E_{qm}^c \end{bmatrix} = \begin{bmatrix} E_p^a \\ E_p^b \\ E_p^c \end{bmatrix} - \begin{bmatrix} Z_{pq}^a & Z_{pq}^{ab} & Z_{pq}^{ac} \\ Z_{pq}^{ab} & Z_{pq}^b & Z_{pq}^{bc} \\ Z_{pq}^{ac} & Z_{pq}^{bc} & Z_{pq}^c \end{bmatrix} \left(\begin{bmatrix} i^a & 0 & 0 \\ 0 & i^b & 0 \\ 0 & 0 & i^c \end{bmatrix} \begin{bmatrix} I_m^a \\ I_m^b \\ I_m^c \end{bmatrix} - \begin{bmatrix} B_p^a & B_p^{ab} & B_p^{ac} \\ B_p^{ab} & B_p^b & B_p^{bc} \\ B_p^{ac} & B_p^{bc} & B_p^c \end{bmatrix} \begin{bmatrix} E_{p0}^a \\ E_{p0}^b \\ E_{p0}^c \end{bmatrix} \right)$$

Average 24-hour load in winter



Linear Method

- ## • Get linear equations

Branch with perfect PT

$$(Y_{12} + B_{12})E_1 = i_{12}I_{12} + Y_{12}e_2E_2$$

$$Y_{12}E_1 = -i_{21}I_{21} + (Y_{12} + B_{12})e_2E_2$$

Branch with two buses to be calibrated

$$0 = -i_{rs} I_{rs} + (Y_{rs} + B_{rs}) e_r E_r - Y_{rs} e_s E_s$$

$$0 = -i_{sr} I_{sr} + (Y_{rs} + B_{rs}) e_s E_s - Y_{rs} e_r E_r$$

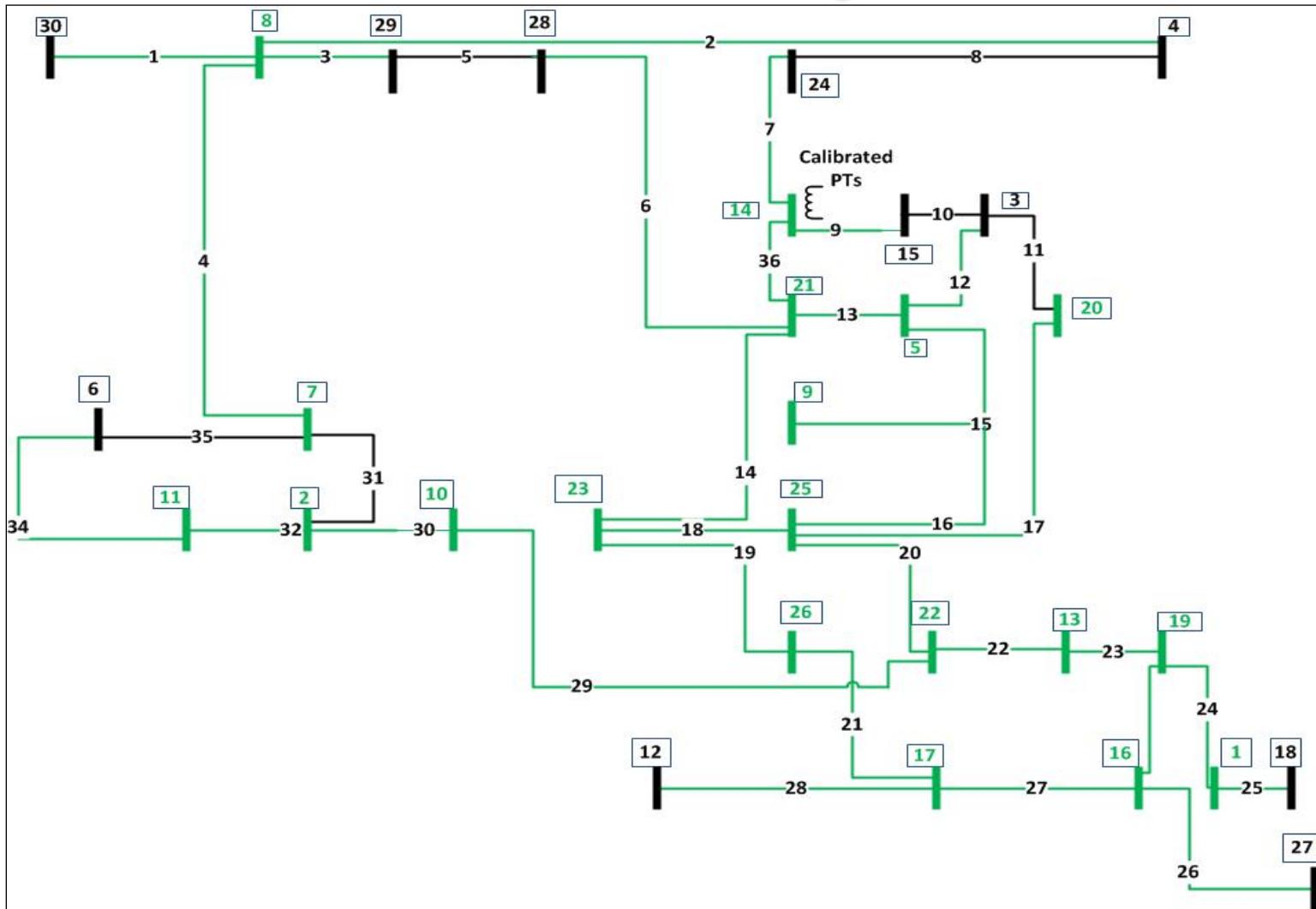
D(I)

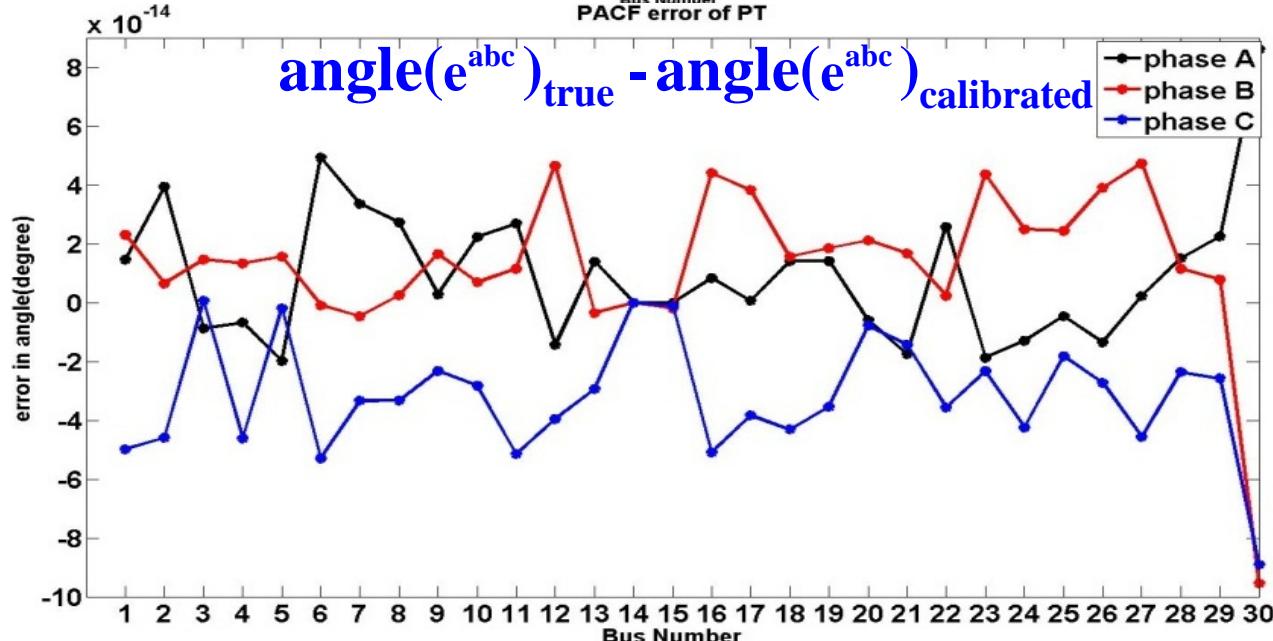
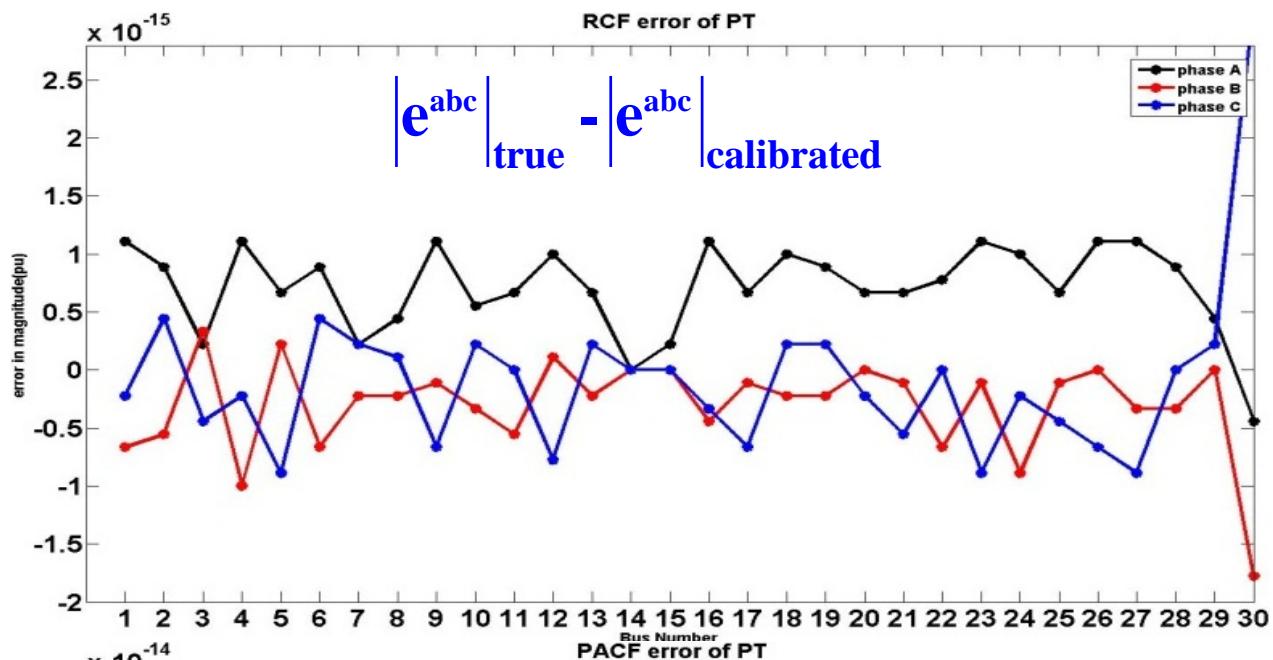
A large blue rectangular box with a black border. Inside the box, the letters 'Y_A E' are written in a white, sans-serif font. The box is positioned in the center of the slide.

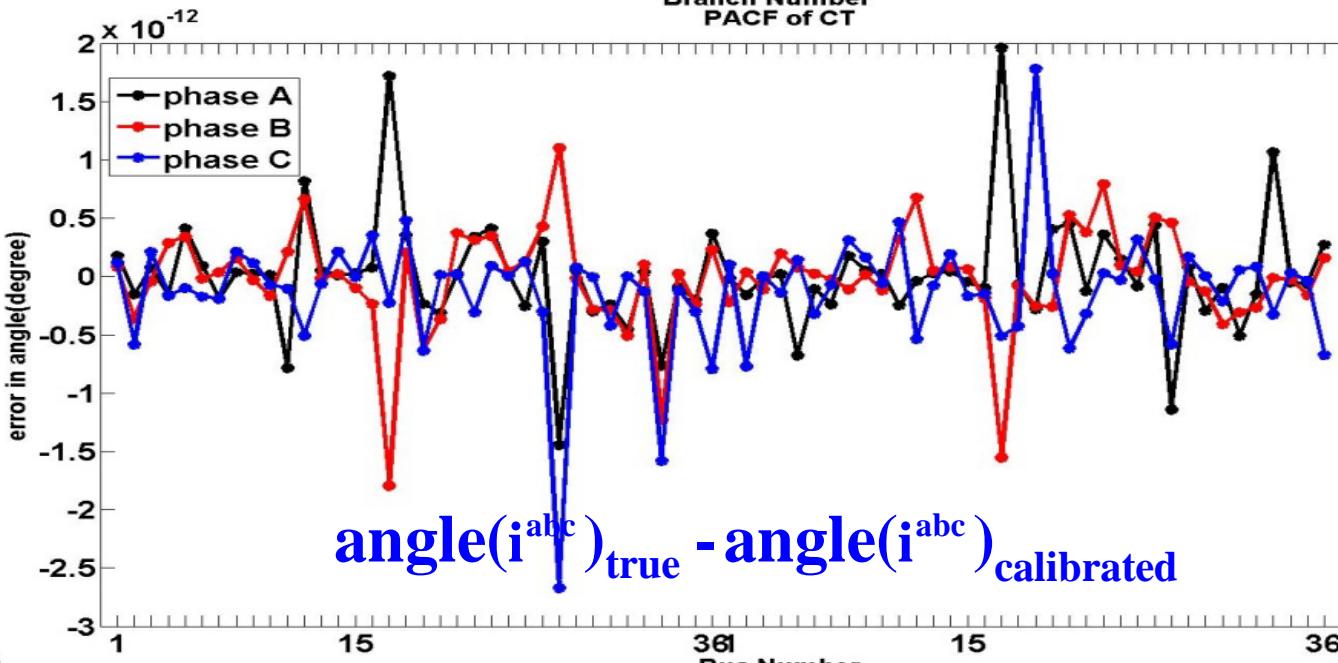
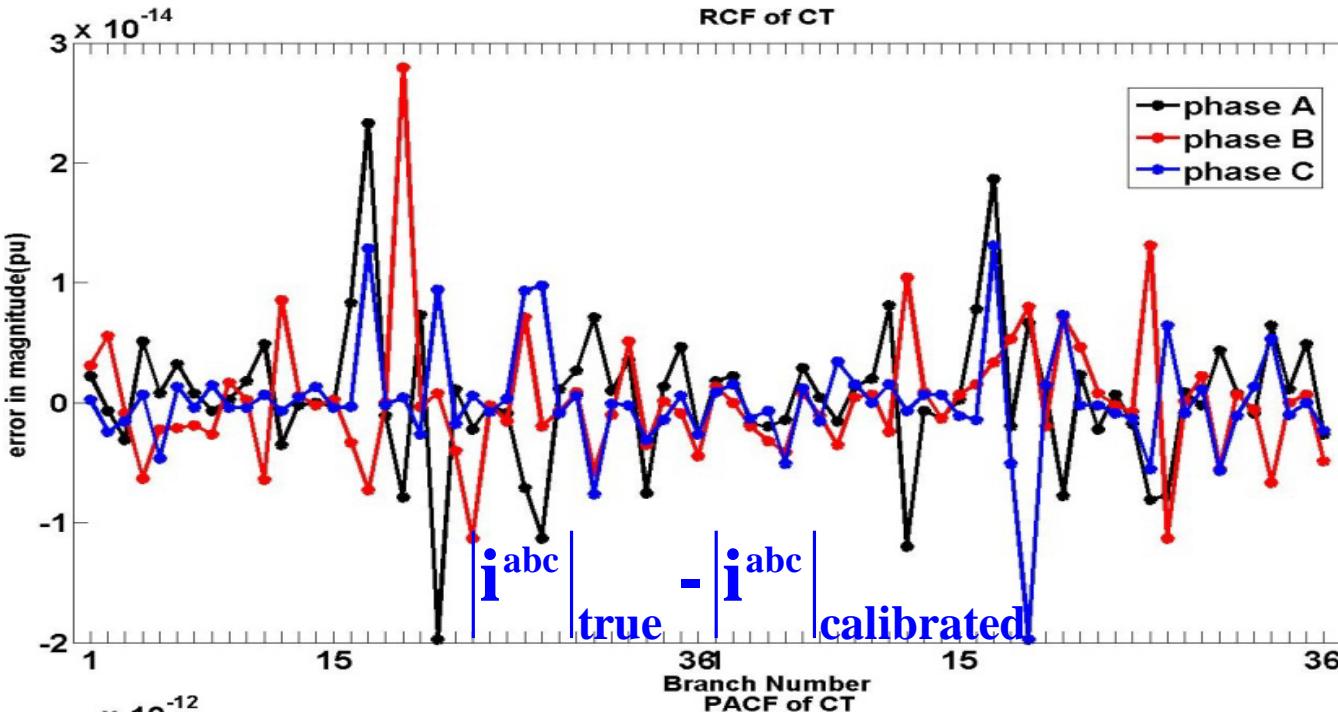
$$\begin{bmatrix} s \\ i_{12} \\ i_{21} \\ i_{rs} \\ i_{sr} \\ \vdots \\ e_2 \\ e_r \\ e_s \\ \vdots \end{bmatrix} = \boxed{E_{ref}}$$

$$X = (D(I) Y_A E)^{-1} E_{ref}$$

DVP 500kv system







Conclusion

- In two-bus system, with perfect voltages at one bus and enough redundancy provided by measurements, the other bus voltage and branch currents can be calibrated.
- Key point: with one bus voltage calibrated, the other voltage and current can be calibrated. Power system is fully connected, then the calibration process can pass from one two-bus to the connected two-bus to the next, throughout the whole system.

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