

# Least costly probing signal design for power system mode estimation

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*Ampère*



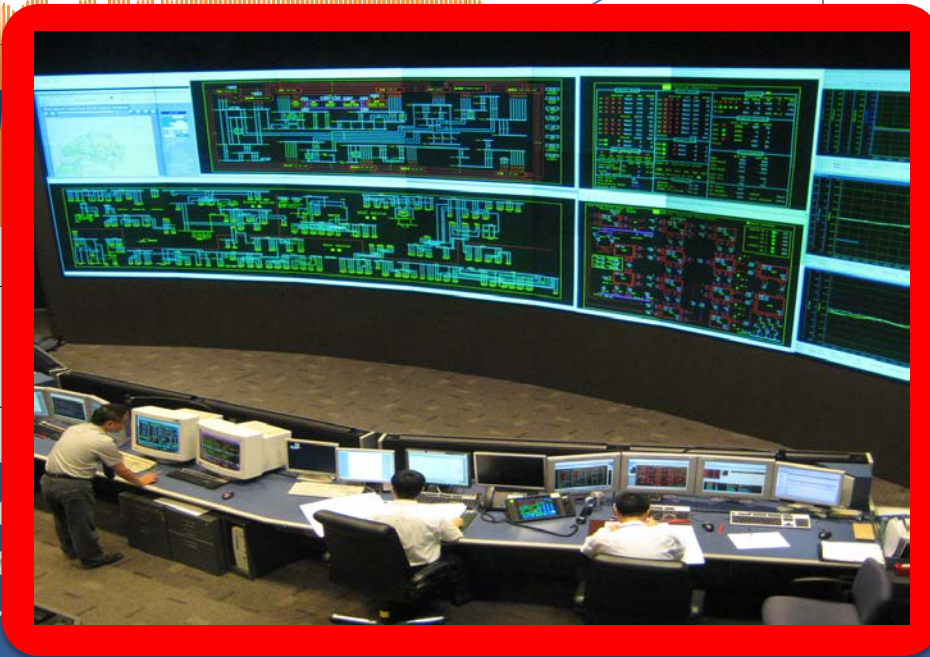
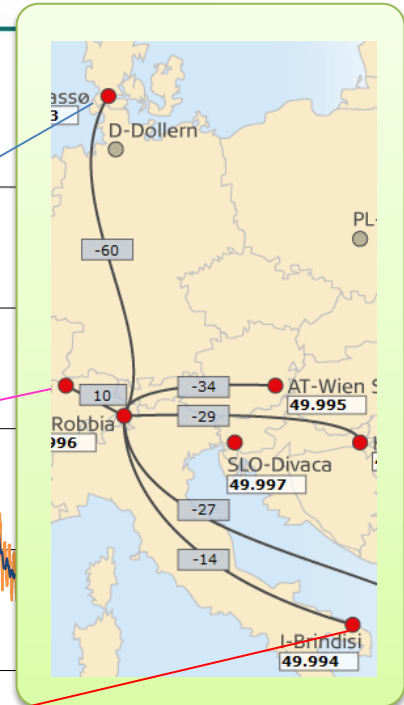
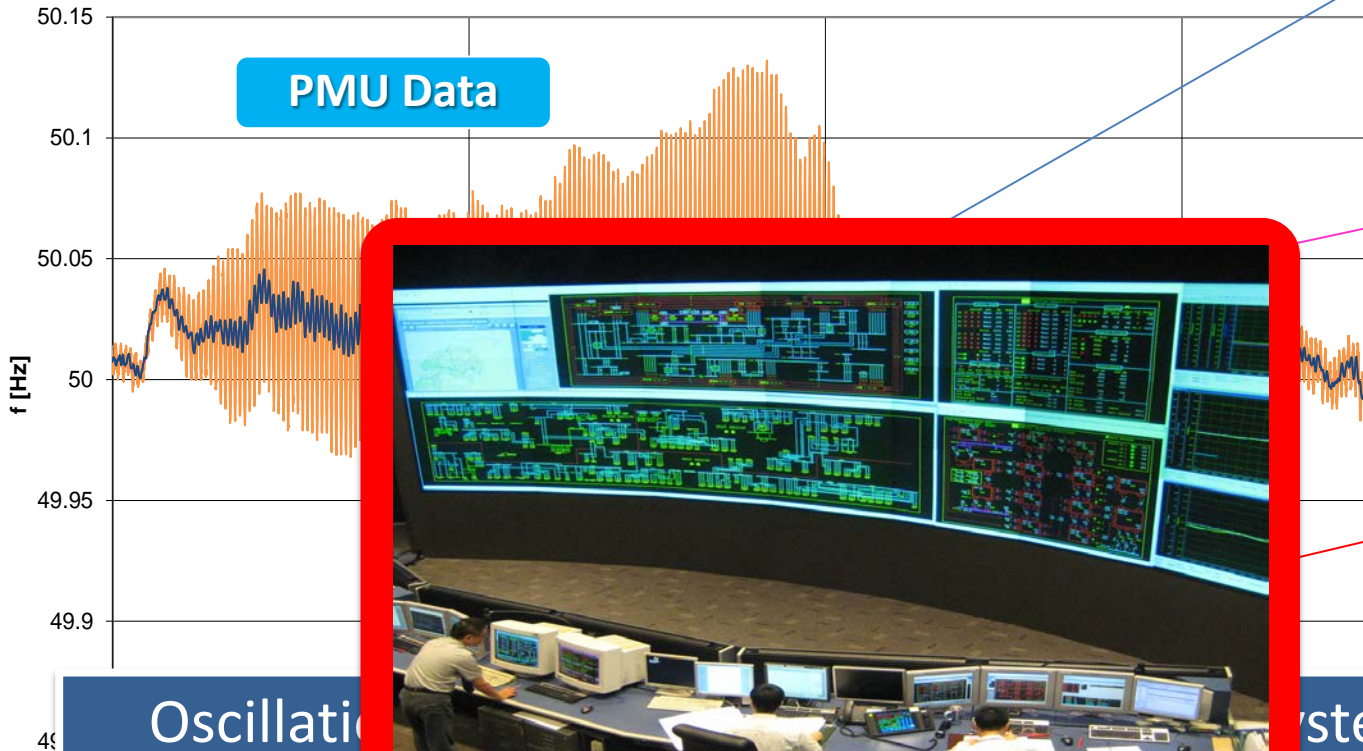
**NASPI Meeting, March 23, 2015.**

# Outline

- Motivation
- Probing-based mode estimation
- Optimization problem formulation
- Results
- Conclusions
- Q&A

# Oscillation monitoring

20110219\_0755-0825  
February 19th 2011 – North-South Inter-Area Oscillation

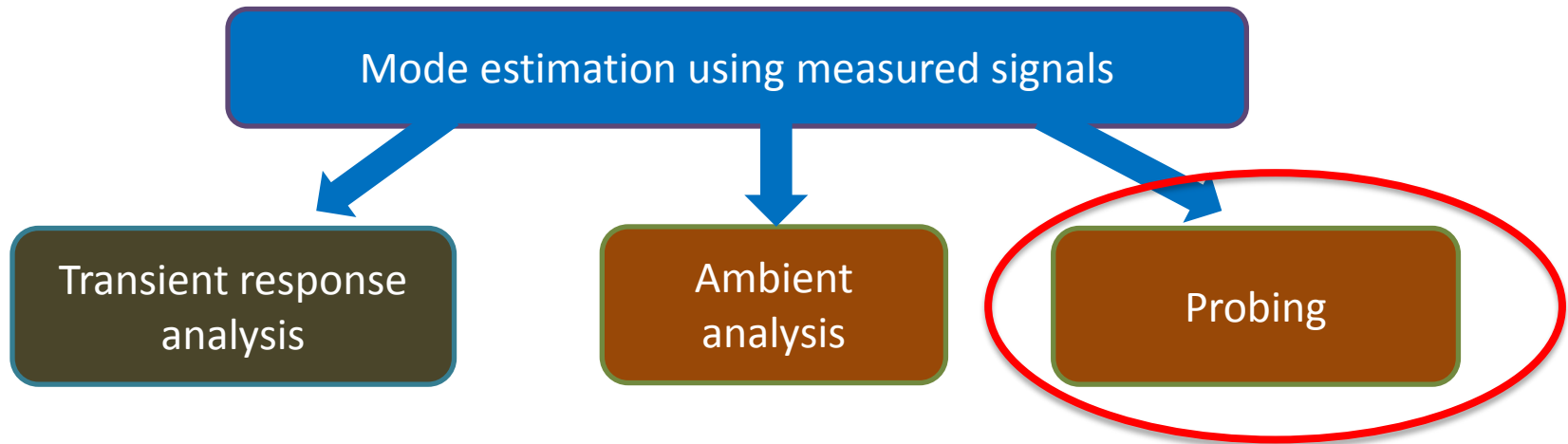


Oscillation system black-out

Oscillation and increase losses

Frequency and damping ratio monitoring

# Algorithms for measurement based mode estimation



- Transient response:

- Prony, ERA, Pencil Matrix
- Well established
- Good accuracy
- Not suitable for real-time monitoring

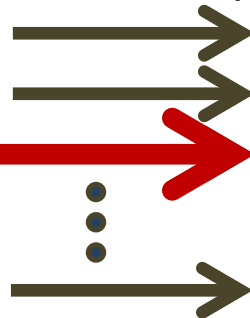
- Ambient and probing :

- SysID and signal processing algorithms
- Suitable for real-time monitoring
- Lower accuracy

# Probing based mode estimation

Inputs

(load noise)

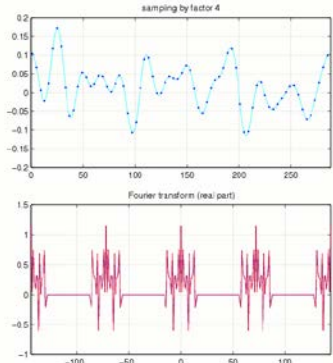
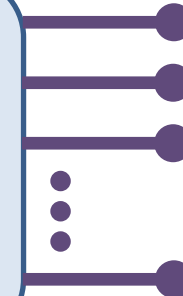


Power system

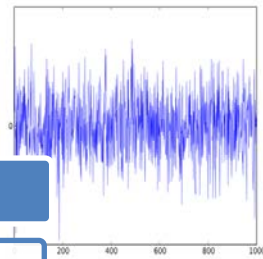
$$\frac{dx}{dt} = Ax + Bu + Fz$$

$$y = Cx + Du + Gz$$

Outputs  
(PMUs)



Deterministic  
signal

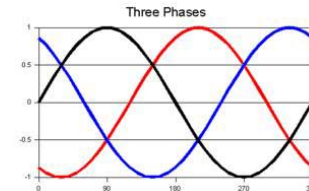
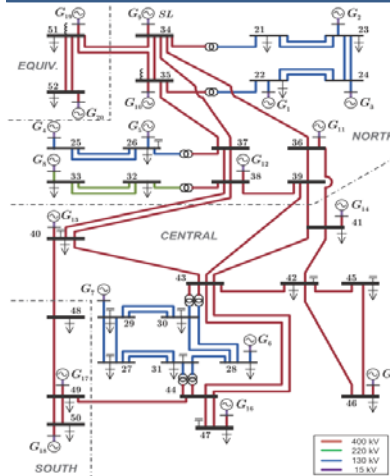


Probing signals

FACTS devices

AVR

Turbine governors

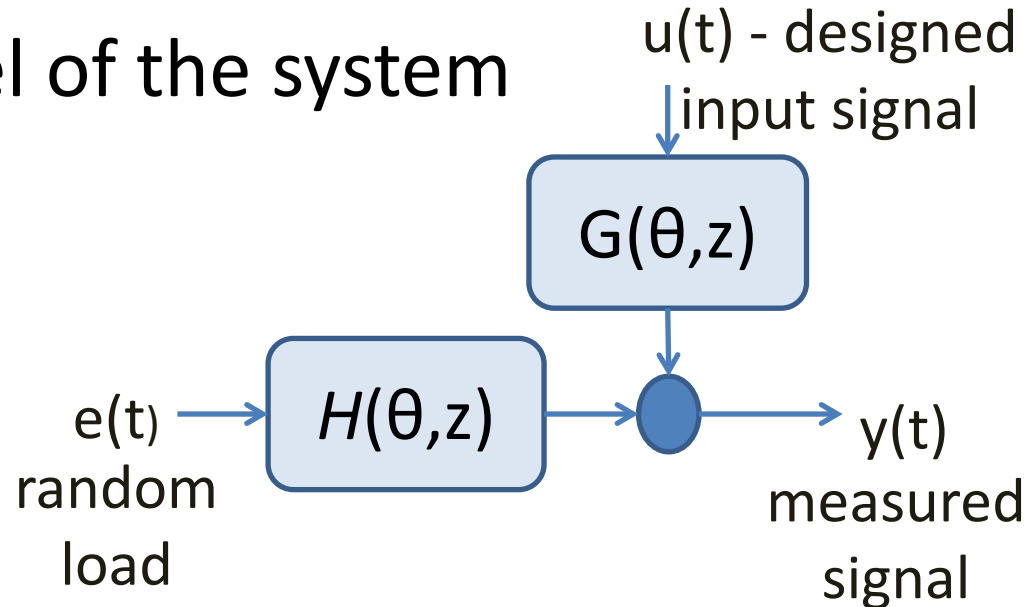


Measured  
signals

**Exactly known excitation brings new information that can be used for improved mode identification**

# Mathematical description of the probing-based mode estimation

- Model of the system



- In case of probing, the model is:
  - ✓ ARMAX
  - ✓ Box Jenkins

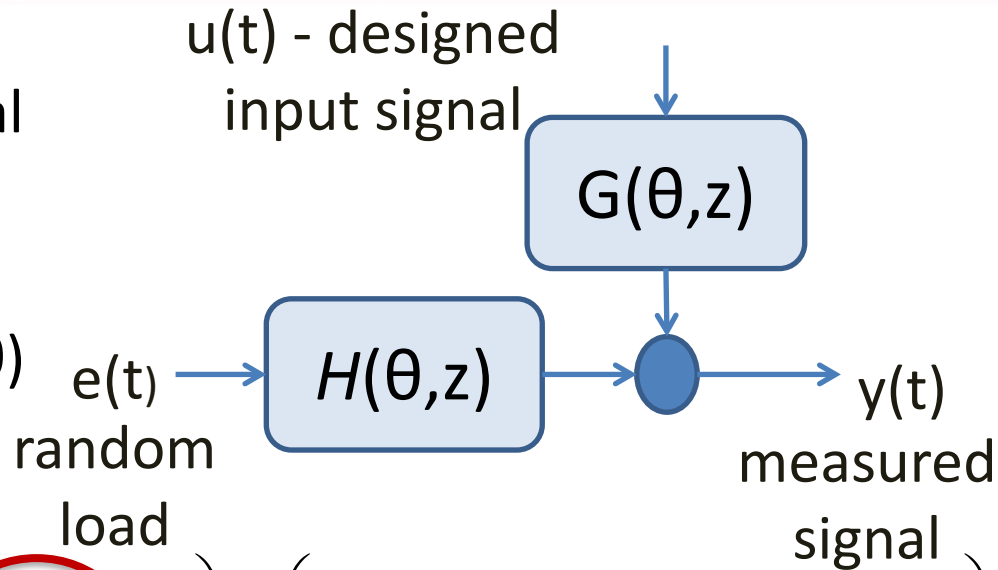
$$y(t) = \frac{B(z, \theta)}{A(z, \theta)} u(t) + \frac{C(z, \theta)}{D(z, \theta)} e(t)$$

- Mode estimation as an optimization problem

$$\min_{\theta} \frac{1}{N} \sum_{t=1}^N \varepsilon(t, \theta)^2 \quad \varepsilon(t, \theta) = y(t) - \widehat{y}(t|t-1)$$

# Parameter covariance matrix

- The goal is to identify the critical damping ratio of  $G(z)$
- The critical damping ratio is parameter of  $G(z)$  (element of  $\theta$ )



$$P_{\theta}^{-1} = \left( \frac{N}{\sigma^2} \frac{1}{2\pi} \int_{-\pi}^{\pi} F_u(\omega, \theta_0) F_u^*(\omega, \theta_0) \Phi_u(\omega) d\omega \right) + \left( \frac{N}{2\pi} \int_{-\pi}^{\pi} F_e(\omega, \theta_0) F_e^*(\omega, \theta_0) d\omega \right)$$

***How should the probing signal look like ???***

- 1) Length
- 2) Frequency spectrum
- 3) Time domain

# Spectrum calculation

## Requirements :

- 1) Control effort      2) System disturbance      3) Accuracy

**Opt. criterion:**

$$\min_{u(t)} J = \underbrace{\left( \frac{k_1}{2\pi} \int_{-\pi}^{\pi} \Phi_u(\omega) d\omega \right)}_{\text{Input}} + \underbrace{\left( \frac{k_2}{2\pi} \int_{-\pi}^{\pi} |G(s)|^2 \Phi_u(\omega) d\omega \right)}_{\text{Output (frequency deviation)}}$$

**Constraint:**       $\text{var}(\zeta_i) = \mathbf{e}_i^T \mathbf{P}_\theta \mathbf{e}_i < r$        $r$  - tolerance

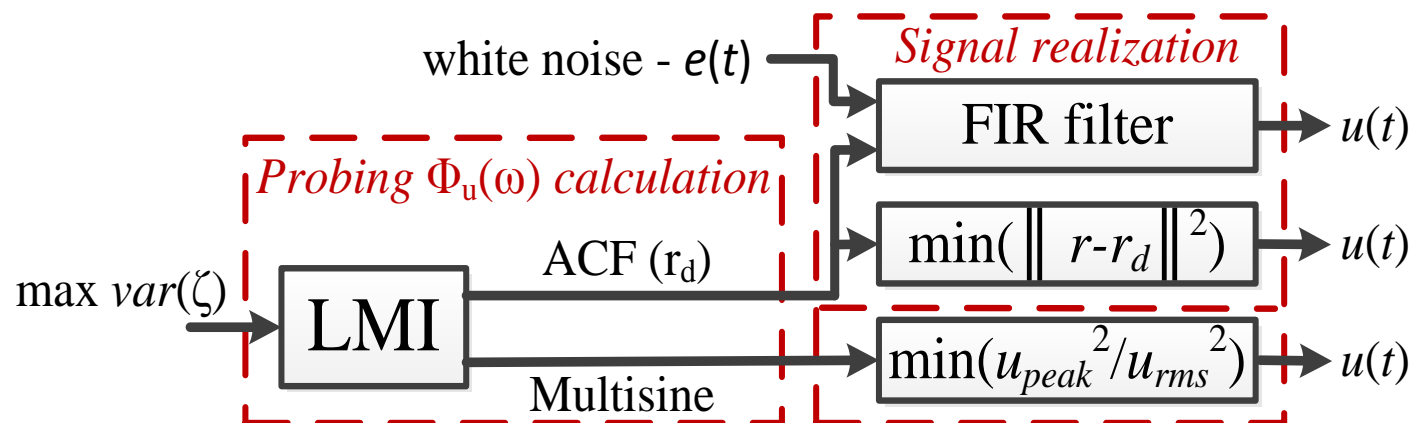
Keeping in mind:

$$\mathbf{P}_\theta^{-1} = \left( \frac{N}{\sigma^2} \frac{1}{2\pi} \int_{-\pi}^{\pi} F_u(\omega, \theta_0) F_u^*(\omega, \theta_0) \Phi_u(\omega) d\omega \right) + \left( \frac{N}{2\pi} \int_{-\pi}^{\pi} F_e(\omega, \theta_0) F_e^*(\omega, \theta_0) d\omega \right)$$



# Global algorithm (two steps)

- Spectrum calculation (LMI optimization)
- Time domain signal realization
  - FIR filter
  - Sample autocorrelation optimization
  - Multi-sine input signal [1]



[1] J.W. Pierre, et al. "Probing signal design for power system identification", *IEEE Trans. Power Syst.*, vol.25, no.2, pp.835-843, May 2010.

# Signal realization with constrained magnitude

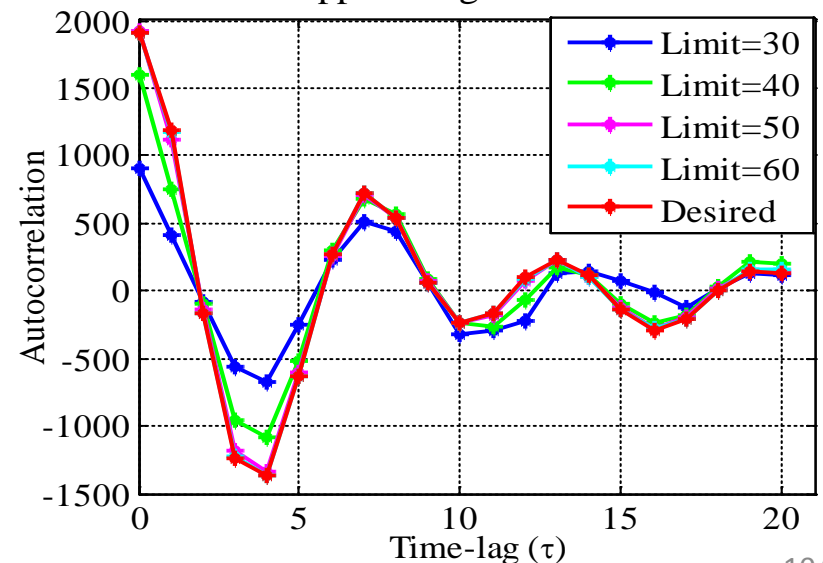
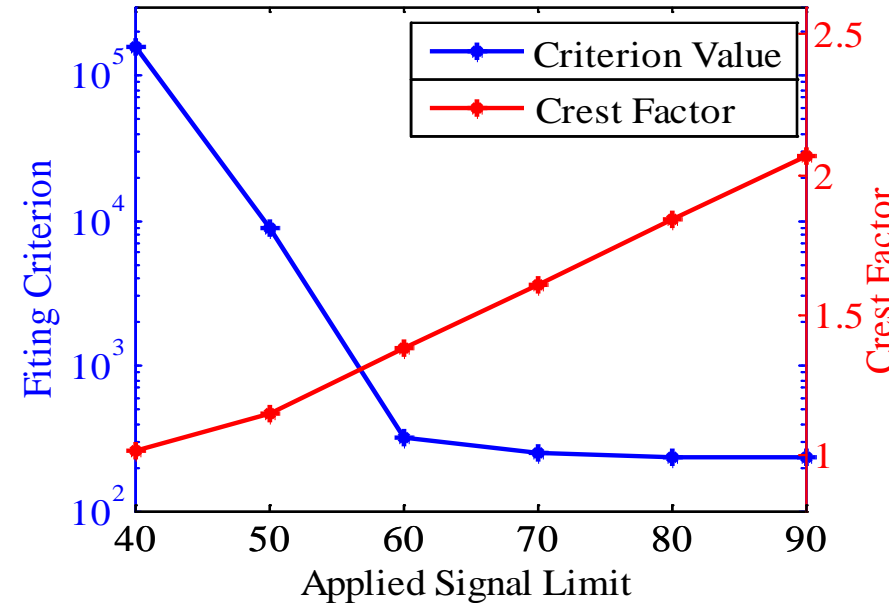
- Power spectrum  $\Phi_u(\omega) = \sum_{r=-m}^m c_r e^{j\omega r}$
- Sample autocorrelation

$$ACF_k(\tau) = \frac{1}{k} \sum_{i=\tau+1}^k u(i)u(i-\tau)$$

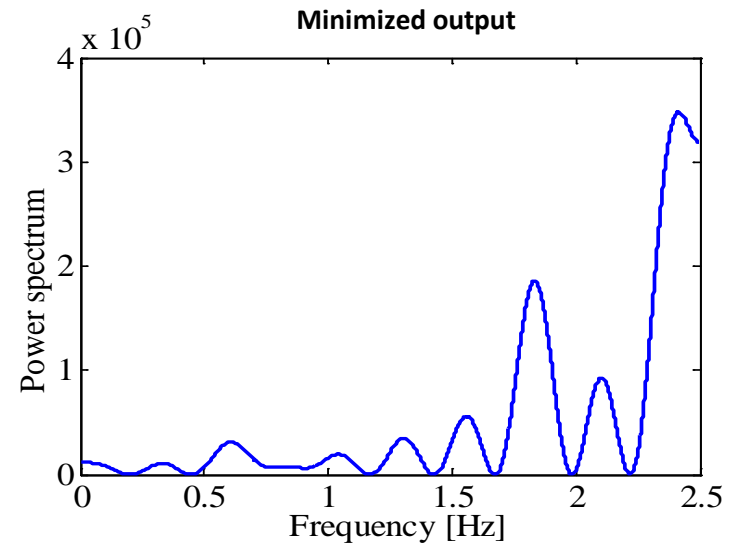
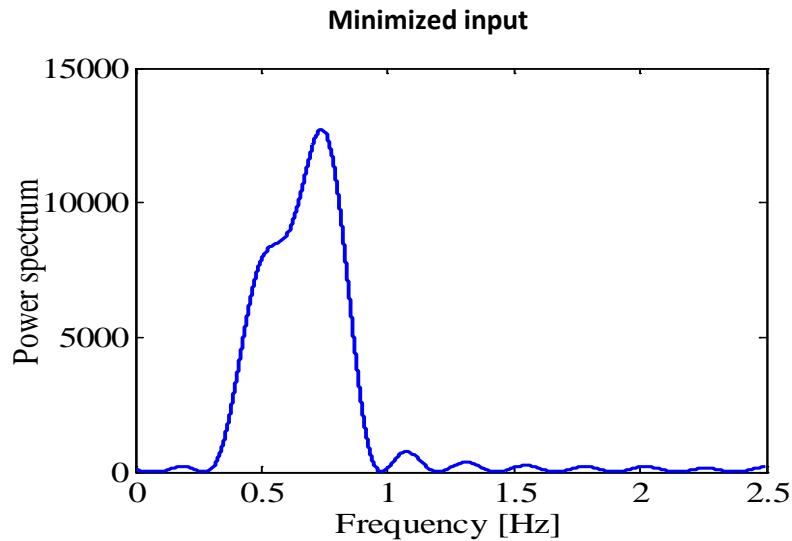
- Optimization

$$\min_{u(k)} \sum_{\tau=0}^{M+K} (ACF_k(\tau) - ACF_{des}(\tau))^2$$

- Efficient recursive algorithm
  - Sample by sample
  - Every sample result of a simple optimization problem



# Optimal probing signal design results



	Input spectrum parameterization		
	White noise	Multi-sine	FIR filter
$\text{var}\{u(t)\}$	10 410.00	1 441.58	1 933.55
$\text{var}\{y(t)\}$	1.67	1.59	1.55
$\text{var}\{u_y(t)\}$	6 881.10	2 318.81	2 518.24

***Optimal probing allows us to reduce probing power and/or system disturbance while maintaining desired accuracy***

# Conclusions

- Monitoring of electromechanical modes is important
- Staged probing tests can provide a good accuracy
- Shape of the probing signal affects estimation accuracy
- Several considerations can be taken into account during design process
- Optimal probing allows us to reduce probing power and/or system disturbance while maintaining accuracy
- The proposed method is easy to implement





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# Thank you!

## Questions?



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